

Lecture 5

ASSIGNMENT

READ "EPI PULSES" PAGES 129-133
"EDDY CURRENT COMPENSATION" PAGES 316-331

LAST TIME

2D SPIRAL PULSES

TODAY

PRACTICAL ISSUES IN 2D SPIRAL PULSE DESIGN

NEXT

EPI AND SPECTRAL SPATIAL PULSES

SUMMARY OF 2D SPIRAL PULSE DESIGN

1) DESIGN A SPIRAL K-SPACE TRAJECTORY $\underline{k}(t)$

RESOLUTION $\Delta r = \frac{1}{2k_{max}}$

FOV $FOV = 2N\Delta r$ (N TURN SPIRAL)

2) DESIGN GRADIENT WAVEFORM

$$\underline{G}(t) = \frac{d}{dt} \underline{k}(T(t))$$

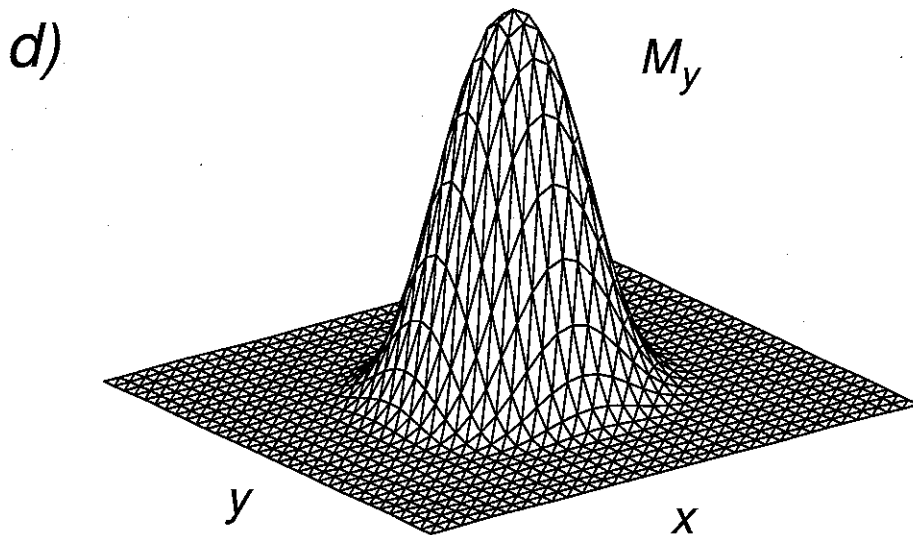
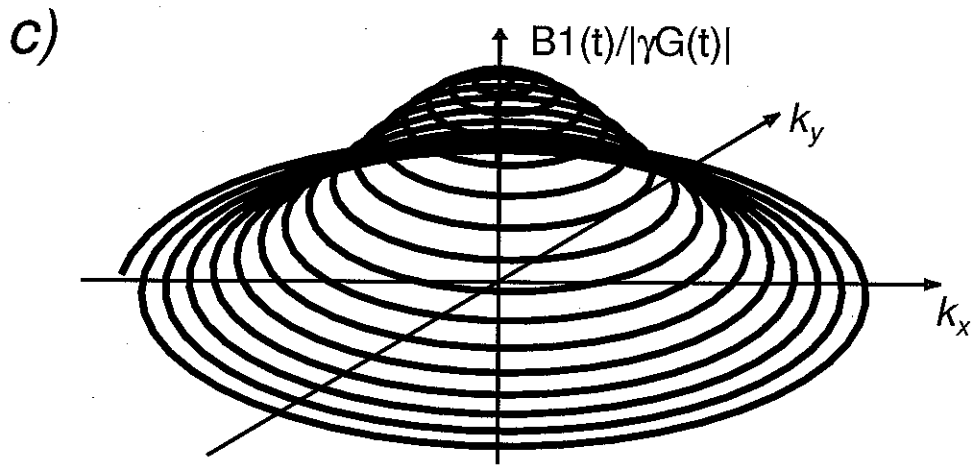
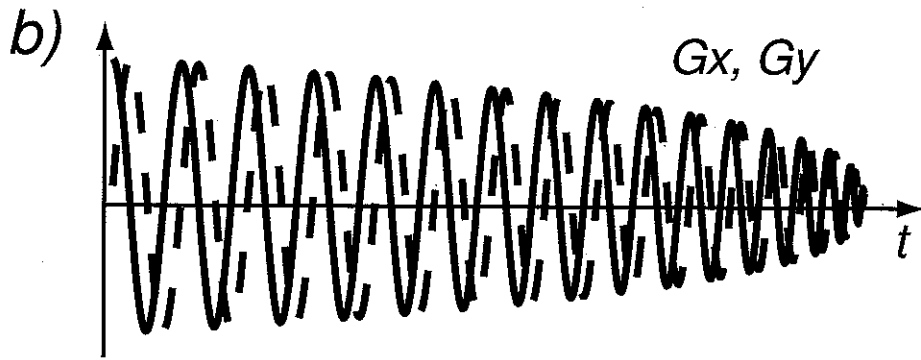
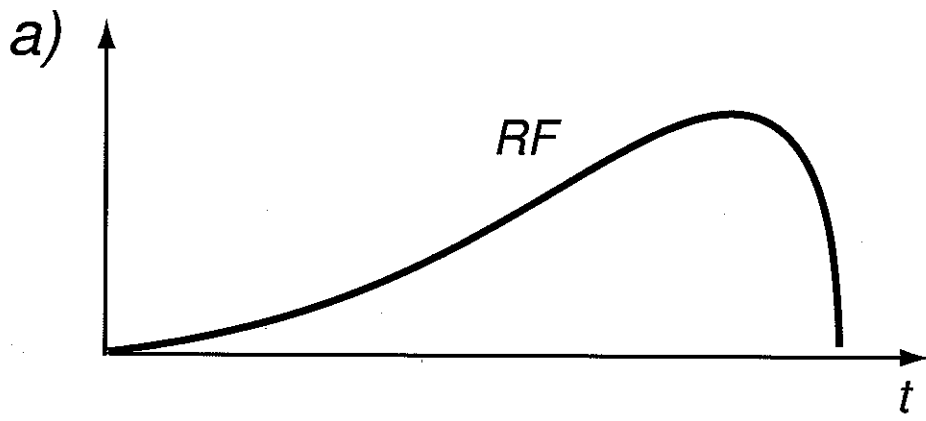
OPTIMIZE $T(t)$ TO MEET AMPLITUDE AND SLEW RATE LIMITS

3) DESIGN K-SPACE WEIGHTING $W(\underline{k})$ AS THE FOURIER TRANSFORM OF THE VOLUME TO BE EXCITED

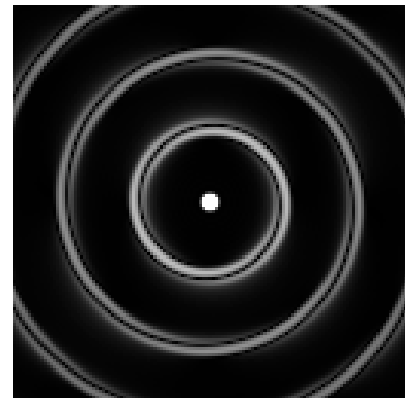
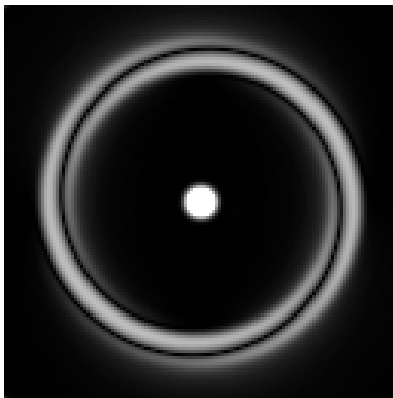
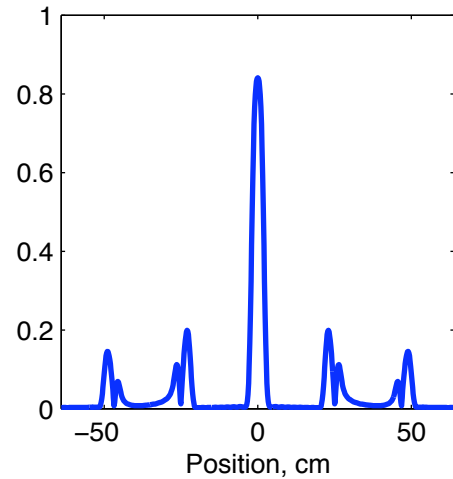
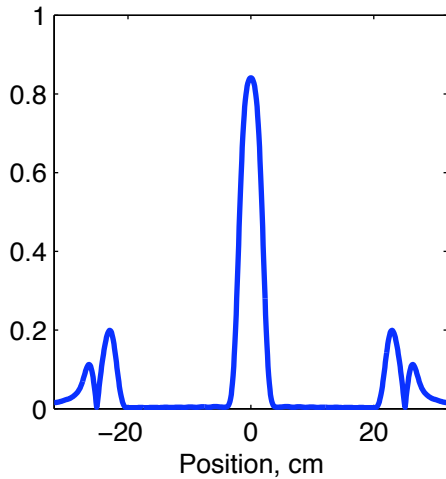
4) CALCULATE THE RF WAVEFORM

$$B_1(t) = |G(t)| W(\underline{k}(T(t)))$$

THEN SCALE TO THE DESIRED FLIP ANGLE



Sidelobe Geometry



*12 turn spiral, 4.5 ms, constant slew rate
1 cm resolution ($k_{max} = +/- 0.5$ cycles/cm)
SBW = 4
Windowed jinc RF*

Sidelobes at +/- 24 cm, +/- 48 cm

BETTER DENSITY COMPENSATION

EXCITED VOLUME

$$m_{xy}(\underline{r}, t) = i m_0 \int_{\underline{k}} P(\underline{k}) e^{i 2\pi \underline{k} \cdot \underline{r}} d\underline{k}$$

WHERE

$$P(\underline{k}) = \int_{-\infty}^t \underbrace{\frac{\gamma B_z(\tau)}{|k'(\tau, t)|}}_{W(\underline{k})} \underbrace{\delta(\underline{k}(\tau, t) - \underline{k})}_{\text{UNIT STREAM DELTA } S(\underline{k})} |k'(\tau, t)| d\tau$$

THE VALUE OF $|k'(\tau, t)|$ IS AN APPROXIMATION OF THE DENSITY COMPENSATION FUNCTION FOR $\underline{k}(\tau, t)$

WHEN $|k'(\tau, t)|$ IS SMALL, WE NEED $B_z(\tau)$ TO ALSO BE SMALL TO PRODUCE CORRECT $W(\underline{k})$

IF WE HAVE AN ESTIMATE OF THE DENSITY $d(\tau)$ FROM SOME ALGORITHM (VONONOI, FOR EXAMPLE), THE DENSITY COMPENSATION FUNCTION IS $\frac{1}{d(\tau)}$ AND

$$|k'(\tau, t)| \sim \frac{1}{d(\tau)}$$

THEN

$$W(\underline{k}(\tau, t)) = \frac{\gamma B_z(\tau)}{1/d(\tau)}$$

$$\underline{B_z(\tau)} = \frac{1}{\gamma} \frac{W(\underline{k}(\tau, t))}{d(\tau)}$$

WHERE $d(\tau)$ IS LOCAL SAMPLE DENSITY.

SHIFTING THE VOLUME

EXCITED VOLUME

$$M_{xy}(\underline{r}, t) = i m_0 \int_{-\infty}^t \gamma B_1(\tau) e^{i 2\pi \underline{K}(\tau, t) \cdot \underline{r}} d\tau$$

WITH MODULATED RF

$$B_{1,m}(\tau) = B_1(\tau) e^{-i 2\pi \underline{K}(\tau, t) \cdot \underline{r}_0}$$

WE GET

$$\begin{aligned} M_{xy,m}(\underline{r}, t) &= i m_0 \int_{-\infty}^t \gamma B_1(\tau) e^{-i 2\pi \underline{K}(\tau, t) \cdot \underline{r}_0} e^{+i 2\pi \underline{K}(\tau, t) \cdot \underline{r}} d\tau \\ &= i m_0 \int_{-\infty}^t \gamma B_1(\tau) e^{i 2\pi \underline{K}(\tau, t) \cdot (\underline{r} - \underline{r}_0)} d\tau \\ &= M_{xy}(\underline{r} - \underline{r}_0, t) \end{aligned}$$

SAME PROFILE, SHIFTED TO \underline{r}_0 .

NOTE THAT WE CAN APPLY

$$\phi(\tau) = -2\pi \underline{K}(\tau, t) \cdot \underline{r}_0$$

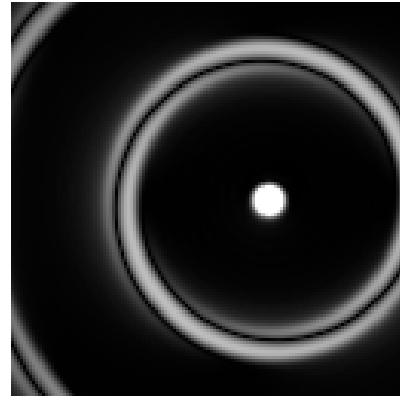
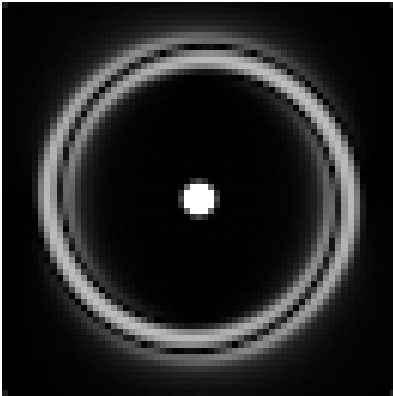
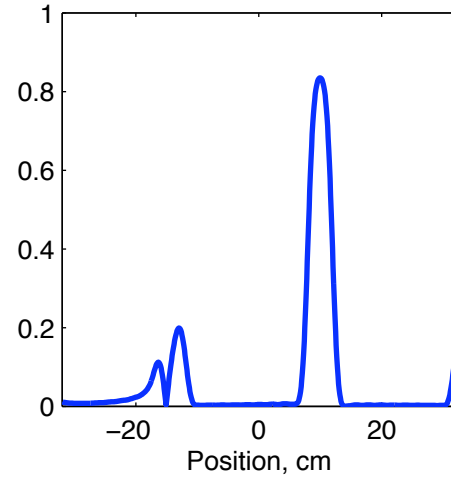
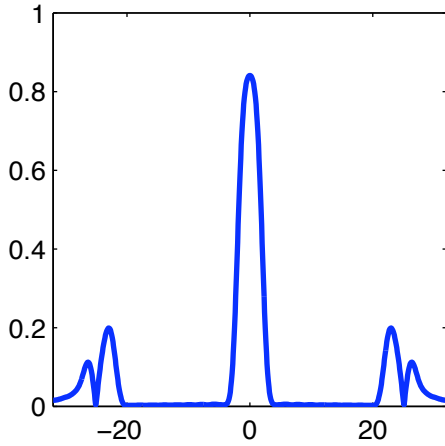
TO THE PHASE CHANNEL, OR

$$\begin{aligned} \omega(\tau) &= \phi'(\tau) = \frac{d}{d\tau} (-2\pi \underline{K}(\tau, t) \cdot \underline{r}_0) \\ &= \frac{d}{d\tau} \left(-2\pi \frac{\lambda}{2\pi} \int_{\tau}^t \omega(s) ds \right) \cdot \underline{r}_0 \\ &= \gamma \underline{G}(\tau) \cdot \underline{r}_0 \end{aligned}$$

TO THE FREQUENCY CHANNEL.

Modulation to Shift FOV

$$B_{1,m}(\tau) = B_1(\tau)e^{-i2\pi k(\tau,t)\cdot r_0}$$



12 turn spiral

1 cm resolution ($k_{max} = \pm 0.5$ cycles/cm)

SBW = 4

Windowed jinc RF

Modulated to +10 cm along x

PRACTICAL CONCERNS: GRADIENT DELAYS

TIME LAG BETWEEN WHEN GRADIENT WAVEFORM IS REQUESTED, AND WHEN SOMETHING HAPPENS IN THE MAGNET BORE

MANY CAUSES, ALL LUMPED TOGETHER

DIGITAL DELAYS IN WAVEFORM GENERATION

FREQUENCY RESPONSE OF GRADIENT COIL / AMPLIFIER

EDDY CURRENTS

TYPICAL NUMBERS ARE 40 μ s TO 150 μ s ON A WHOLE BODY SYSTEM.

WHAT DOES THIS DO TO 2D SPIRAL EXCITATION PULSES?

CONSTANT ANGULAR RATE SPIRAL

ASSUME WE DESIGNED A 2D SPIRAL PULSE
WITH THE CONSTANT ANGULAR RATE TRAJECTORY

$$\underline{k}(t) = k_{\max} \left(1 - \frac{t}{T}\right) e^{i 2\pi N \left(1 - \frac{t}{T}\right)}$$

AND AN ASSOCIATED $B_s(t)$.

IF THE GRADIENT IS DECAYED BY A TIME δ

$$\underline{k}(t-\delta) = k_{\max} \left(1 - \frac{t-\delta}{T}\right) e^{i 2\pi N \left(1 - \frac{t-\delta}{T}\right)}$$

IF δ IS SMALL

$$\begin{aligned} \underline{k}(t-\delta) &\approx k_{\max} \left(1 - \frac{t}{T}\right) e^{i 2\pi N \left(1 - \frac{t}{T}\right)} e^{i 2\pi N \delta / T} \\ &= \underline{k}(t) e^{i 2\pi N \delta / T} \end{aligned}$$

RECALL THAT

$$\underline{k}(t) = k_x(t) + i k_y(t)$$

MULTIPLICATION BY $e^{i 2\pi N \delta / T}$ IS A ROTATION
OF THE k -SPACE TRAJECTORY BY

$$\underline{\theta} = \underline{2\pi N \delta / T} \quad \text{RADIAN}$$

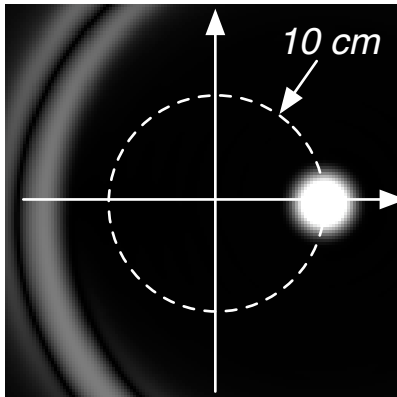
EXAMPLE: 12 TURN SPIRAL, 4.5ms LONG
GRADIENT DELAY OF 16μs

$$\theta = 2\pi(12) \frac{0.016}{4.5} = 0.27 \text{ RADIANs}$$
$$= \underline{\underline{15^\circ}}$$

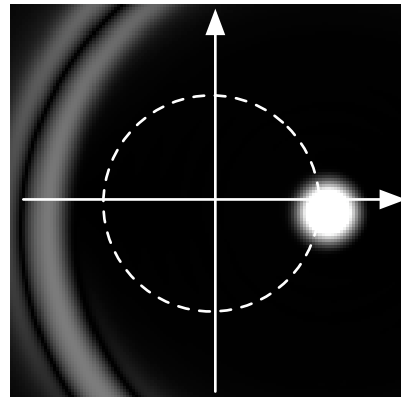
RESULT: GRADIENT DELAY CAUSES ROTATION
ABOUT THE ISOCENTER PRIMARILY, WITH
LITTLE OTHER DISTORTION

*Effect of Gradient Delay:
Constant Angular Rate Spiral*

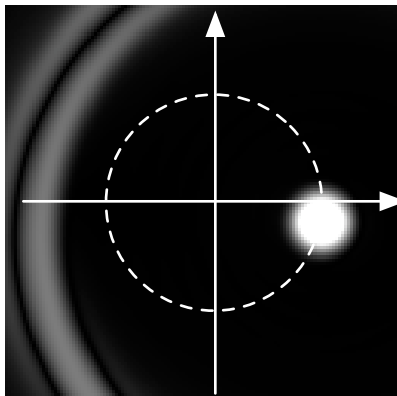
No Delay



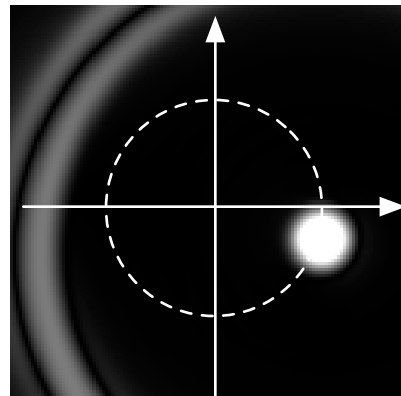
4 us



8 us



16 us



12 turn spiral, 6.5 ms, constant angular rate

1 cm resolution ($k_{max} = \pm 0.5$ cycles/cm)

SBW = 4

Windowed sinc RF

Modulated to +10 cm along x

Delay Produces:

Rotation about isocenter

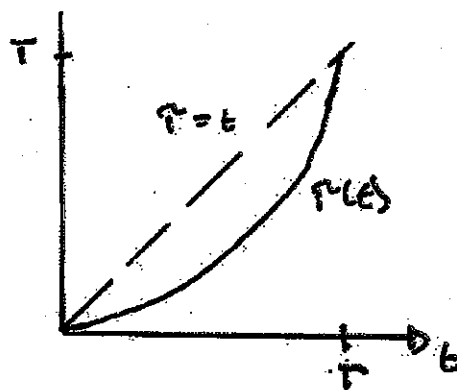
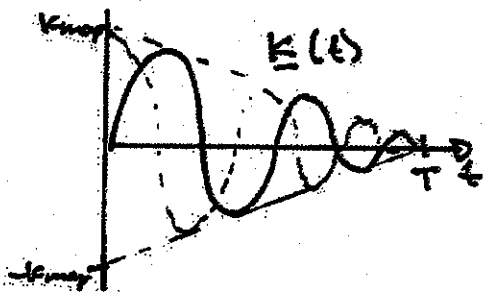
GRADIENT / SUEW OPTIMIZED SPIRAL

Now

$$\underline{k}(r(t)) = k_{max} \left(1 - \frac{r(t)}{T}\right) e^{i2\pi N \left(1 - \frac{r(t)}{T}\right)}$$

LET s BE THE GRADIENT DELAY

$$\underline{k}(r(t-s)) = k_{max} \left(1 - \frac{r(t-s)}{T}\right) e^{i2\pi N \left(1 - \frac{r(t-s)}{T}\right)}$$



IF s IS SMALL, $r(t)$ SMOOTH, SLOWLY VARYING

$$\begin{aligned} \underline{k}(r(t-s)) &\approx k_{max} \left(1 - \frac{r(t)}{T}\right) e^{i2\pi N \left(1 - \frac{r(t-s)}{T}\right)} \\ &= k_{max} \left(1 - \frac{r(t)}{T}\right) e^{i2\pi N \left(1 - \frac{r(t)}{T}\right)} e^{i2\pi N s r(t)/T} \\ &= \underline{k}(r(t)) e^{i2\pi N s r(t)/T} \end{aligned}$$

AGAIN, THIS IS A ROTATION BUT IS DEPENDENT ON TIME / SPATIAL FREQUENCY

EACH SPATIAL FREQUENCY ROTATED BY A DIFFERENT AMOUNT \Rightarrow DISPERSION

ROTATION ANGLE

$$\theta(\epsilon) = 2\pi N \delta T(\epsilon) / T \text{ RADIANS}$$

RESULT:

HIGH SPATIAL FREQUENCIES

LARGE GRADIENT AMPLITUDES

PLAYED OUT SLOWER

LESS ROTATION

LOW SPATIAL FREQUENCIES

SMALL GRADIENT AMPLITUDES

PLAYED OUT FASTER

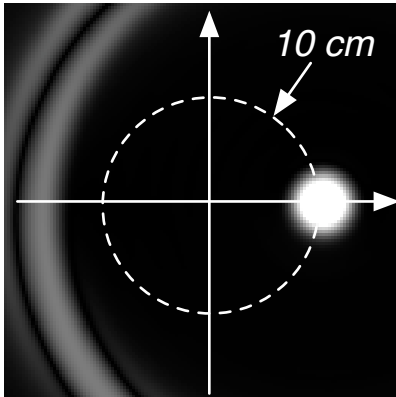
MORE ROTATION

HIGH AND LOW SPATIAL FREQUENCIES

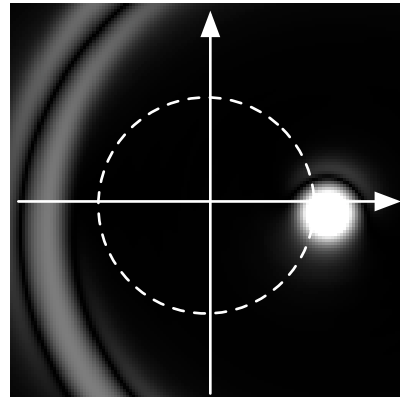
GET OUT OF ALIGNMENT

*Effect of Gradient Delay:
Constant Slew Rate Spiral*

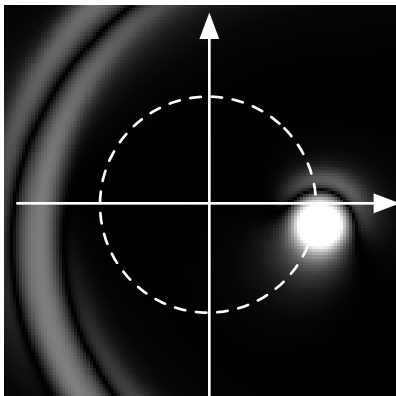
No Delay



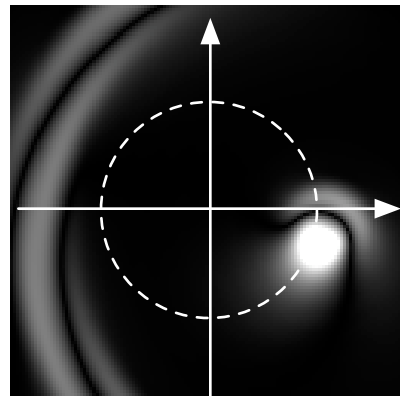
4 us



8 us



16 us



*12 turn spiral, 4.5 ms, constant slew rate
1 cm resolution ($k_{max} = \pm 0.5$ cycles/cm)
SBW = 4
Windowed jinc RF
Modulated to +10 cm along x*

Delay Produces:

Rotation about isocenter

Distortion of the selected volume

OFF-RESONANCE EFFECTS

MANY SOURCES OF B_0 VARIATIONS

MAIN FIELD INHOMOGENEITY

SUBJECT SUSCEPTIBILITY

CHEMICAL SHIFT

EDDY CURRENTS

HOW DO THESE EFFECT TO SPIRAL PULSES?

IDEALLY THE k -SPACE WEIGHTING IS

$$W(k) = \frac{\delta R_1(k)}{|k|}$$

IF THE RF IS APPLIED AT AN OFF-RESONANCE FREQUENCY ω , THE ACTUAL WEIGHTING IS

$$W_a(k) = \frac{\delta R_1(k) e^{-i\omega t}}{|k|}$$

FOR A CONSTANT ANGULAR RATE INWARD SPIRAL

$$k(t) = k_{max} \left(1 - \frac{t}{T}\right) e^{i2\pi \omega (1 - t/T)}$$

$$|k(t)| = k_{max} \left(1 - \frac{t}{T}\right)$$

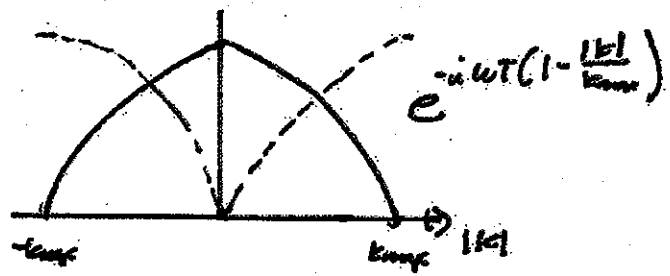
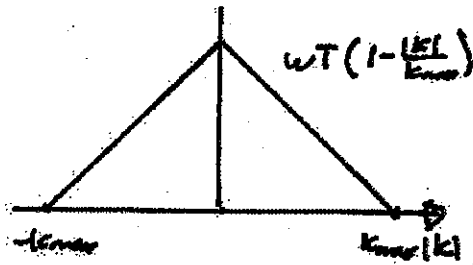
$$t = T \left(1 - \frac{|k|}{k_{max}}\right)$$

THEN

$$W_a(\underline{k}) = \frac{D B_1(\underline{k})}{18 G(\underline{k})} e^{-i\omega T(1 - \frac{|\underline{k}|}{k_{max}})}$$

$$W_a(\underline{k}) = \underbrace{W(\underline{k})}_{\substack{\text{DESIRABLE} \\ \text{WEIGHTING}}} e^{-i\omega T(1 - \frac{|\underline{k}|}{k_{max}})} \underbrace{\phantom{e^{-i\omega T(1 - \frac{|\underline{k}|}{k_{max}})}}}_{\substack{\text{PHASE} \\ \text{ABERRATION}}}$$

EFFECT OF PHASE ABERRATION



SMALL AMOUNT OF ABERRATION (LESS THAN SBW/4 CYCLES)

BLURRING OF IMPULSE RESPONSE

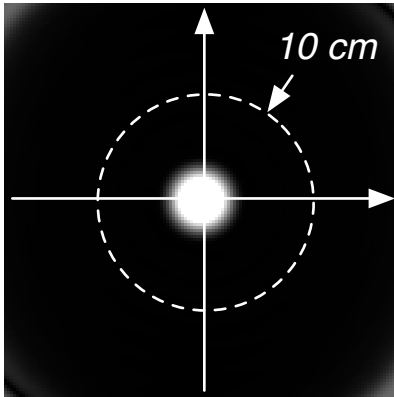
SIGNIFICANT ABERRATION (MORE THAN SBW/4 CYCLES)

SIGNIFICANT BLURRING

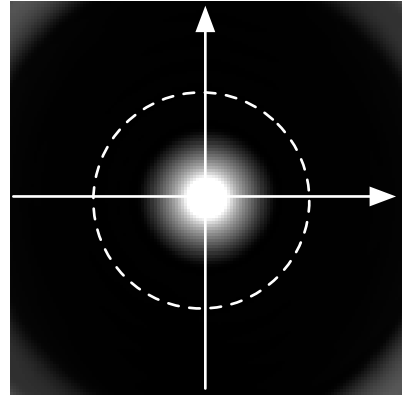
LOSS OF AMPLITUDE

Effect of Off-Resonance

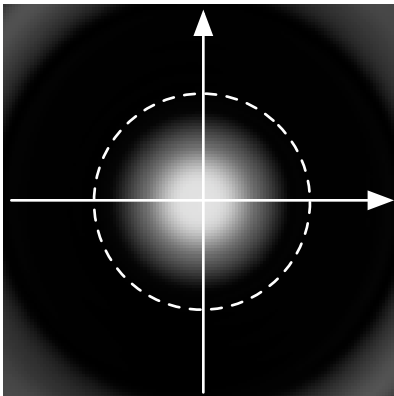
On Resonance



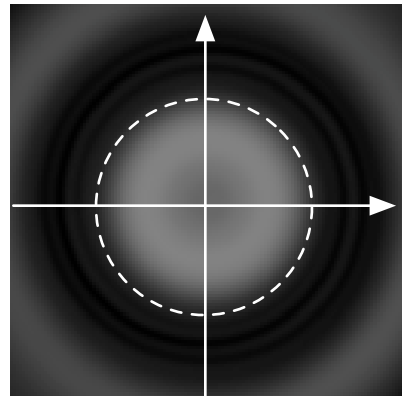
220 Hz



440 Hz

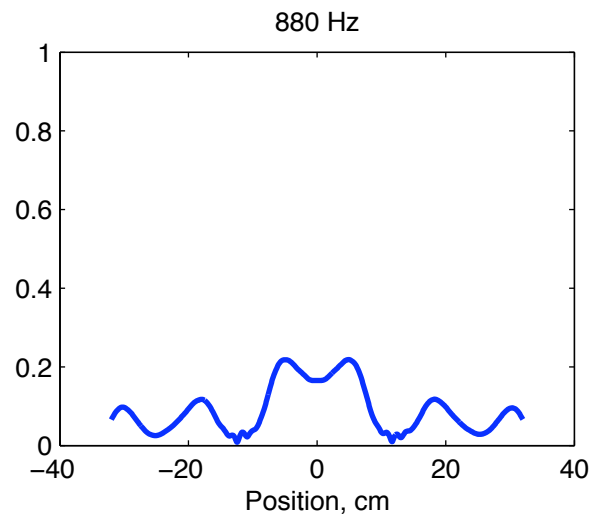
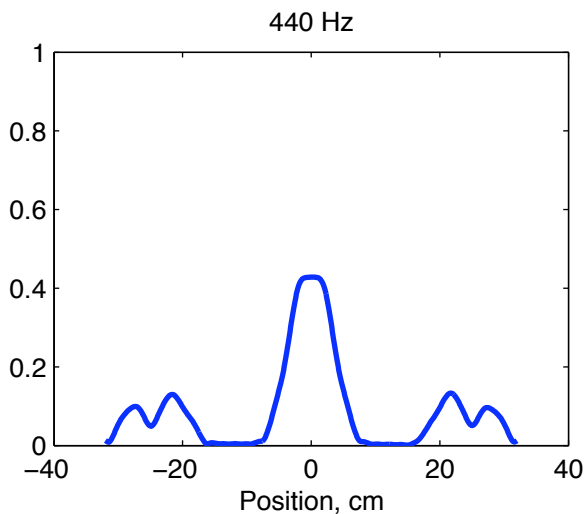
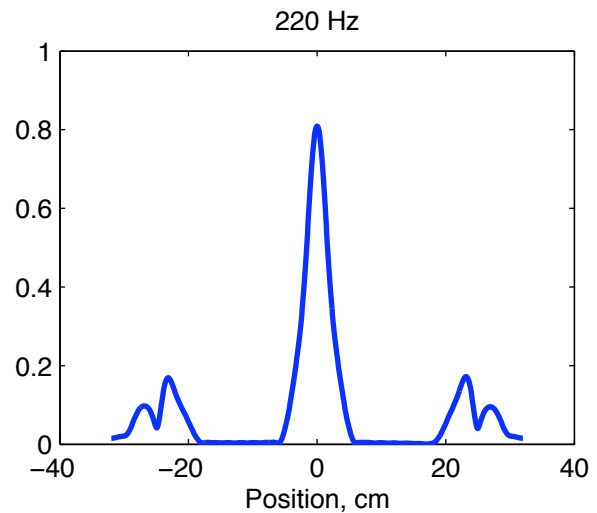
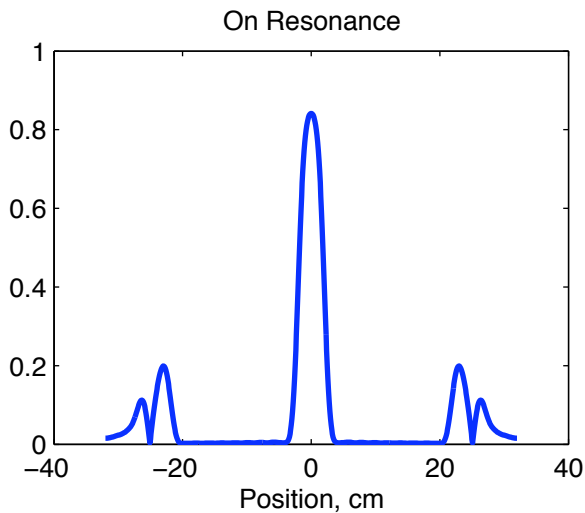


880 Hz



*12 turn spiral, 4.5 ms, constant slew rate
1 cm resolution ($k_{max} = \pm 0.5$ cycles/cm)
SBW = 4
Windowed jinc RF
220 Hz is one cycle over pulse length*

Effect of Off-Resonance



*12 turn spiral, 4.5 ms, constant slew rate
1 cm resolution ($k_{max} = \pm 0.5$ cycles/cm)
SBW = 4
Windowed jinc RF
220 Hz is one cycle over pulse length*